# The Distillery Traffic Access Study 

## Prepared For:

GeoGraphics, Inc.

Prepared By:


SURVEYING•ENGINEERING•ENVIRONMENTAL
S E R V I C E S

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# The Distillery Traffic Access Study 

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## Under the direction of:



$$
\frac{6-09-2022}{\text { Date }}
$$



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## BACKGROUND

AB Contracting, Inc. is proposing to develop a site with 232 multifamily units. The site is located on the south side of SR 752 between Reynolds Road and Long Street (between the railroad overpass and the railroad at grade crossing). Figure 1 shows the location of the site. There is one proposed access on SR 752. The Village is also requiring the developer to connect and perform some upgrades to an existing access road to the east of the site. For purposes of the TAS, all traffic is assumed to utilize the SR 752 access. Figure 2 shows the site layout. The annexation for this property extends to the centerline of SR 752 so the permitting agency for the access is the Village of Ashville. It is our understanding that they are requiring a traffic access study (TAS). Because half of the road is outside the Village, the Ohio Department of Transportation (ODOT) will also have review of the TAS.

## EXISTING CONDITIONS

SR 752 in the area of the site is a two-lane road with a posted speed limit of 55 MPH. Table 1 summarizes the data being used as the basis of the existing traffic as well as the traffic control. Per the ODOT State Highway Access Management Manual, a factor must be applied to the count to convert it to a design hour. This factor was applied to both peak hours and based on ODOT's Peak Hour to Design Hour Factors chart. SR 752 is classified as Major Collector (FC 5). The Major Collector Factors (in Appendix) were applied. The factor associated with a Thursday in March is 1.23.

| SEGMENT |  |  | PM |
| :---: | :---: | :---: | :---: |
|  | SOURCE | AM | PEAK |
|  |  | PEAK HOUR | PEAUR |
| SR 752 | Smart | $3 / 03 / 2022$ | $3 / 03 / 2022$ |
|  | Services, Inc. | $6: 45-7: 45$ AM | $4: 30-5: 30$ PM |

TABLE 1 - Summary of Existing Traffic Basis


## PROJECTED SITE TRAFFIC

## Trip Generation

In traffic engineering, the accepted method for computing trip generation is utilizing data from the Trip Generation Manual, $11^{\text {th }}$ Edition published by the Institute of Transportation Engineers. Table 2 shows the trip generation calculations.

## Trip Distribution

The distribution of traffic was assumed to be the same as the existing distribution in the PM Peak which is as follows:
-45\% - To/from the east on SR 752
$\bullet 55 \%$ - To/from the west on SR 752

## 2023 \& 2033 TRAFFIC

A 10-Year design horizon is required by ODOT for this level of development. Opening Day is assumed to be 2023; therefore, the design year is 2033. The growth rates were obtained from the ODOT TIMS website. The printout from TIMS is in the Appendix. Table 3 shows the growth rates and corresponding factors applied to the 2022 counts.

| SEGMENT | LINEAR <br> ANNUAL <br> GROWTH <br> RATE | 2022 TO <br> 2023 <br> FACTOR | 2022 TO <br> 2033 <br> FACTOR |
| :---: | :---: | :---: | :---: |
| SR 752 | $2.79 \%$ | 1.028 | 1.307 |

TABLE 3 - Growth Factor Summary for 2022 Counts
Figures 3 and 4 show the components of the 2023 'Build' traffic. Figures 5 and 6 show the components of the 2033 'Build' traffic.

|  | LAND USE | TIME OF DAY | DATA SET <br> Trip Generation Manual, 11th <br> Edition <br> (Unless noted Otherwise) | RATE OR EQUATION <br> FROM: <br> Trip Generation <br> Manual <br> 11th Edition | TOTAL TRIPS | ENTERING |  | EXITING |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SUBAREA |  |  |  |  |  | \% | TOTAL TRIPS | \% | TOTAL TRIPS |
| 1 | Multifamily Housing (Low-Rise) Not Close to Rail/Transit (ITE Code \#220) | Daily | Weekday | $\mathrm{T}=6.41(\mathrm{X})+75.31$ | 1562 | 50\% | 781 | 50\% | 781 |
|  |  | AM Peak | Peak Hour of Adj. Street Traffic, One Hour between 7 \& 9 AM | $\mathrm{T}=0.31(\mathrm{X})+22.85$ | 95 | 24\% | 23 | 76\% | 72 |
|  | Ind. Variable ( X ) = 232 Dwelling Units | PM Peak | Peak Hour of Adj. Street Traffic, One Hour between 4 \& 6 PM | $\mathrm{T}=0.43(\mathrm{X})+20.55$ | 120 | 63\% | 76 | 37\% | 44 |
| TOTALS |  | Daily |  |  | 1562 |  | 781 |  | 781 |
|  |  | AM Peak |  |  | 95 |  | 23 |  | 72 |
|  |  | PM Peak |  |  | 120 |  | 76 |  | 44 |

TABLE 2 - SITE TRIP GENERATION SUMMARY

| L | A (SHEET TITLE $)=\mathrm{B}+\mathrm{C}+\mathrm{D}+\mathrm{E}$ |
| :--- | :--- |
| E | = EXISTING (2022) |
|  | C = DHF ADJUSTMENT |
| G | D = GROWTH |
| E | E SITE TOTAL |
| N |  |
| D |  |



NOTE: Existing AM Peak volumes have been adjusted to account for the dhf.

NOTE: Rounding as a result of software algorithms can result in one car discrepancies in the site traffic between intersections.

THE DISTILLERY

> L A (SHEET TITLE) $=\mathrm{B}+\mathrm{C}+\mathrm{D}+\mathrm{E}$
> E $\quad$ B = EXISTING (2022)
> C = DHF ADJUSTMENT
> G $\quad$ D = GROWTH
> E E SITE TOTAL
> N
> D


NOTE: Existing PM Peak volumes have been adjusted to account for the dhf.

NOTE: Rounding as a result of software algorithms can result in one car discrepancies in the site traffic between intersections.

```
L A (SHEET TITLE) \(=\mathrm{B}+\mathrm{C}+\mathrm{D}+\mathrm{E}\)
E B = EXISTING (2022)
C = DHF ADJUSTMENT
G \(\mathrm{D}=\mathrm{GROWTH}\)
E E = SITE TOTAL
N
D
```



NOTE: Existing AM Peak volumes have been adjusted to account for the dhf.

NOTE: Rounding as a result of software algorithms can result in one car discrepancies in the site traffic between intersections.

THE DISTILLERY TRAFFIC ACCESS STUDY

> L A (SHEET TITLE) $=\mathrm{B}+\mathrm{C}+\mathrm{D}+\mathrm{E}$
> E $\quad$ B = EXISTING (2022)
> C = DHF ADJUSTMENT
> G $\quad$ D = GROWTH
> E E SITE TOTAL
> N
> D


NOTE: Existing PM Peak volumes have been adjusted to account for the dhf.

NOTE: Rounding as a result of software algorithms can result in one car discrepancies in the site traffic between intersections.

## TRAFFIC ANALYSIS

## Turn Lane Warrant Analysis

The procedure to determine whether turn lanes are warranted is according to the ODOT L\&D Manual published by the Ohio Department of Transportation (ODOT). Since the Village corporation limit is the centerline of SR 752, it is the understanding of Smart Services, Inc. that the developer has received conflicting direction regarding the prima-facie speed limit on SR 752. Therefore, the analysis was considered for both the criteria over and under 40 MPH . The results are shown in Table 4. The graphs from the ODOT L\&D Manual are in the Appendix. Also in Table 4 is the number of units that result in the approximate threshold units for the 2033 'Build’ condition.

| MOVEMENT | 2023 'BUILD' |  | 2033 'BUILD' |  |
| :---: | :---: | :---: | :---: | :---: |
|  | >40 MPH | $\mathbf{= < 4 0 \text { MPH }}$ | $\mathbf{> 4 0}$ MPH | =<40 MPH |
| SR 752 WB left turn <br> at Prop. Site Access | Warrant <br> Met | Warrant <br> Met | Warrant <br> Met <br> $(\approx 70$ Units) | Warrant <br> Met <br> $(\approx 165$ Units) |
| SR 752 EB right turn <br> at Prop. Site Access | Warrant <br> Not Met | Warrant <br> Not Met | Warrant <br> Met <br> $(\approx 165$ Units) | Warrant <br> Not Met |

*=The Village may not require the eastbound right turn lane.
TABLE 4 - Summary of Turn Lane Warrant Analysis

## Turn Lane Length Analysis

Turn lane lengths for the warranted turn lanes per the turn lane analyses were calculated. The calculations were performed per Section 400 of the ODOT L\&D Manual. ODOT has indicated that the prima-facie speed limit is 50 MPH . The design speed is typically assumed to be 5 MPH above the speed limit. Because there is limited space for developing turn lanes between the railroad tracks to the east and west, calculations have been provided for both 50 MPH and 55 MPH . Table 5 shows a summary of the results. The calculations are in the Appendix.

| LOCATION | DIRECTION | SPEED LIMIT/ DESIGN SPEED | 2023 'BUILD' | 2033 'BUILD' |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | ODOT L\&D Manual | ODOT L\&D Manual |
| SR 752$\&$Prop. Site Access | WB LT | 50 / 50 MPH | $\begin{gathered} \hline \hline 225 ’ / 285 ' \\ { }^{\prime} 100^{\prime} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 225 ’ / 285 ' \\ { }^{\prime} 100^{\prime} \\ \hline \end{gathered}$ |
|  | EB RT | 50 / 55 MPH | NA | $\begin{gathered} 225 ’ / 285 ' \\ { }^{\prime} 100^{\prime} \\ \hline \end{gathered}$ |

## CONCLUSIONS

2023 'Build' and 2033 'Build' volumes were developed for use in turn lane warrant and turn lane length analyses. Below is a summary of the conclusions for each condition:

## 2023 'Build'

- SR 752 \& Prop. Site Access
$\circ$ A westbound left turn lane is warranted. For a design speed of 55 MPH, the length of the lane is 285 feet which includes the 50 -foot diverging taper. For a design speed of 50 MPH , the length of the lane is 225 feet which includes the 50 -foot diverging taper. Because of the limited space in this area between the railroad tracks, the developer and ODOT will have to work out the design parameters. $\circ$ An eastbound right turn lane is not warranted.


## 2033 'Build'

-SR 752 \& Prop. Site Access
oA westbound left turn lane is warranted. The threshold occurs at approximately 70 units. For a design speed of 55 MPH , the length of the lane is 285 feet which includes the 50 -foot diverging taper. For a design speed of 50 MPH , the length of the lane is 225 feet which includes the 50 -foot diverging taper. Because of the limited space in this area between the railroad tracks, the developer and ODOT will have to work out the design parameters.
-An eastbound right turn lane is warranted. The threshold occurs at approximately 165 units. For a design speed of 55 MPH, the length of the lane is 285 feet which includes the 50 -foot diverging taper. For a design speed of 50 MPH , the length of the lane is 225 feet which includes the 50 -foot diverging taper. The Village may not require the eastbound right turn lane.

## APPENDIX

SR 752 West of SR 316 (Long St)-Ashville Pike - ATR
Thu Mar 3, 2022
Full Length (6 AM-10 AM, 3 PM-7 PM)
All Classes (Lights and Motorcycles, Heavy)
All Channels
ID: 927598, Location: 39.7235, -82.952874

| $\begin{array}{\|l\|} \hline \text { Leg } \\ \text { Direction } \end{array}$ |  | West <br> Eastbound |  | East <br> Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time |  | T | App | T | App | Int |
|  | 2022-03-03 6:00AM | 18 | 18 | 29 | 29 | 47 |
|  | 6:15AM | 14 | 14 | 33 | 33 | 47 |
|  | 6:30AM | 27 | 27 | 57 | 57 | 84 |
|  | 6:45AM | 34 | 34 | 46 | 46 | 80 |
|  | Hourly Total | 93 | 93 | 165 | 165 | 258 |
|  | 7:00AM | 69 | 69 | 35 | 35 | 104 |
|  | 7:15AM | 85 | 85 | 49 | 49 | 134 |
|  | 7:30AM | 58 | 58 | 36 | 36 | 94 |
|  | 7:45AM | 24 | 24 | 43 | 43 | 67 |
|  | Hourly Total | 236 | 236 | 163 | 163 | 399 |
|  | 8:00AM | 27 | 27 | 33 | 33 | 60 |
|  | 8:15AM | 30 | 30 | 39 | 39 | 69 |
|  | 8:30AM | 35 | 35 | 41 | 41 | 76 |
|  | 8:45AM | 24 | 24 | 42 | 42 | 66 |
|  | Hourly Total | 116 | 116 | 155 | 155 | 271 |
|  | 9:00AM | 37 | 37 | 37 | 37 | 74 |
|  | 9:15AM | 39 | 39 | 35 | 35 | 74 |
|  | 9:30AM | 27 | 27 | 38 | 38 | 65 |
|  | 9:45AM | 27 | 27 | 36 | 36 | 63 |
|  | Hourly Total | 130 | 130 | 146 | 146 | 276 |
|  | 3:00PM | 50 | 50 | 34 | 34 | 84 |
|  | 3:15PM | 29 | 29 | 30 | 30 | 59 |
|  | 3:30PM | 58 | 58 | 52 | 52 | 110 |
|  | 3:45PM | 52 | 52 | 49 | 49 | 101 |
|  | Hourly Total | 189 | 189 | 165 | 165 | 354 |
|  | 4:00PM | 70 | 70 | 59 | 59 | 129 |
|  | 4:15PM | 71 | 71 | 43 | 43 | 114 |
|  | 4:30PM | 63 | 63 | 69 | 69 | 132 |
|  | 4:45PM | 83 | 83 | 48 | 48 | 131 |
|  | Hourly Total | 287 | 287 | 219 | 219 | 506 |
|  | 5:00PM | 82 | 82 | 58 | 58 | 140 |
|  | 5:15PM | 58 | 58 | 57 | 57 | 115 |
|  | 5:30PM | 73 | 73 | 47 | 47 | 120 |
|  | 5:45PM | 76 | 76 | 43 | 43 | 119 |
|  | Hourly Total | 289 | 289 | 205 | 205 | 494 |
|  | 6:00PM | 60 | 60 | 41 | 41 | 101 |
|  | 6:15PM | 54 | 54 | 39 | 39 | 93 |
|  | 6:30PM | 60 | 60 | 32 | 32 | 92 |
|  | 6:45PM | 53 | 53 | 26 | 26 | 79 |
|  | Hourly Total | 227 | 227 | 138 | 138 | 365 |
|  | Total | 1567 | 1567 | 1356 | 1356 | 2923 |
|  | \% Approach | 100\% | - | 100\% | - |  |
|  | \% Total | 53.6\% | 53.6\% | 46.4\% | 46.4\% |  |
|  | Lights and Motorcycles | 1515 | 1515 | 1310 | 1310 | 2825 |
|  | \% Lights and Motorcycles | 96.7\% | 96.7\% | 96.6\% | 96.6\% | 96.6\% |
|  | Heavy | 52 | 52 | 46 | 46 | 98 |
|  | \% Heavy | 3.3\% | 3.3\% | 3.4\% | 3.4\% | 3.4\% |

[^0]SR 752 West of SR 316 (Long St)-Ashville Pike - ATR
Thu Mar 3, 2022
AM Peak (6:45 AM - 7:45 AM)
All Classes (Lights and Motorcycles, Heavy)
All Channels
ID: 927598, Location: 39.7235, -82.952874

| Leg <br> Direction |  | West <br> Eastbound |  | East <br> Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time |  | T | App | T | App | Int |
|  | 2022-03-03 6:45AM | 34 | 34 | 46 | 46 | 80 |
|  | 7:00AM | 69 | 69 | 35 | 35 | 104 |
|  | 7:15AM | 85 | 85 | 49 | 49 | 134 |
|  | 7:30AM | 58 | 58 | 36 | 36 | 94 |
|  | Total | 246 | 246 | 166 | 166 | 412 |
|  | \% Approach | 100\% | - | 100\% | - | - |
|  | \% Total | 59.7\% | 59.7\% | 40.3\% | 40.3\% | - |
|  | PHF | 0.724 | 0.724 | 0.847 | 0.847 | 0.769 |
|  | Lights and Motorcycles | 236 | 236 | 162 | 162 | 398 |
|  | \% Lights and Motorcycles | 95.9\% | 95.9\% | 97.6\% | 97.6\% | 96.6\% |
|  | Heavy | 10 | 10 | 4 | 4 | 14 |
|  | \% Heavy | 4.1\% | 4.1\% | 2.4\% | 2.4\% | 3.4\% |

*T: Thru

SR 752 West of SR 316 (Long St)-Ashville Pike - ATR
Thu Mar 3, 2022
PM Peak (4:30 PM - 5:30 PM) - Overall Peak Hour
All Classes (Lights and Motorcycles, Heavy)
All Channels
ID: 927598, Location: 39.7235, -82.952874

Provided by: Smart Services, Inc.

| $\begin{array}{\|l\|} \hline \text { Leg } \\ \text { Direction } \end{array}$ |  | West <br> Eastbound |  | East <br> Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time |  | T | App | T | App | Int |
|  | 2022-03-03 4:30PM | 63 | 63 | 69 | 69 | 132 |
|  | 4:45PM | 83 | 83 | 48 | 48 | 131 |
|  | 5:00PM | 82 | 82 | 58 | 58 | 140 |
|  | 5:15PM | 58 | 58 | 57 | 57 | 115 |
|  | Total | 286 | 286 | 232 | 232 | 518 |
|  | \% Approach | 100\% | - | 100\% | - |  |
|  | \% Total | 55.2\% | 55.2\% | 44.8\% | 44.8\% |  |
|  | PHF | 0.861 | 0.861 | 0.841 | 0.841 | 0.925 |
|  | Lights and Motorcycles | 279 | 279 | 225 | 225 | 504 |
|  | \% Lights and Motorcycles | 97.6\% | 97.6\% | 97.0\% | 97.0\% | 97.3\% |
|  | Heavy | 7 | 7 | 7 | 7 | 14 |
|  | \% Heavy | 2.4\% | 2.4\% | 3.0\% | 3.0\% | 2.7\% |

${ }^{*} \mathrm{~T}$ : Thru


TIMS
INFORMATION
MAPPING SYSTEM

## PEAK HOUR to DESIGN HOUR FACTORS <br> FUNCTIONAL CLASSIFICATION = 05, 06r <br> (Rural Major Collector \& Rural Minor Collector)

|  | Monthly Average by Day-of-Week |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MONTHUR | Sunday | Monday | Tuesday | Wednesday | Thursday | Friday | Saturday |
| January | 1.31 | 2.00 | 1.35 | 1.32 | 1.29 | 1.28 | 1.23 | 1.80 |
| February | 1.26 | 1.91 | 1.27 | 1.25 | 1.27 | 1.28 | 1.18 | 1.67 |
| March | 1.24 | 1.80 | 1.25 | 1.24 | 1.24 | 1.23 | 1.17 | 1.64 |
| April | 1.16 | 1.60 | 1.20 | 1.18 | 1.13 | 1.14 | 1.08 | 1.55 |
| May | 1.13 | 1.56 | 1.15 | 1.12 | 1.12 | 1.11 | 1.06 | 1.46 |
| June | 1.18 | 1.57 | 1.20 | 1.20 | 1.15 | 1.15 | 1.13 | 1.44 |
| July | 1.22 | 1.60 | 1.25 | 1.22 | 1.20 | 1.22 | 1.17 | 1.50 |
| August | 1.17 | 1.53 | 1.18 | 1.17 | 1.16 | 1.14 | 1.09 | 1.40 |
| September | 1.13 | 1.54 | 1.16 | 1.13 | 1.12 | 1.10 | 1.04 | 1.39 |
| October | 1.13 | 1.59 | 1.17 | 1.11 | 1.12 | 1.11 | 1.04 | 1.39 |
| November | 1.18 | 1.77 | 1.21 | 1.17 | 1.17 | 1.19 | 1.08 | 1.59 |
| December | 1.22 | 1.86 | 1.22 | 1.22 | 1.22 | 1.24 | 1.16 | 1.64 |

peak hour volume * factor = design hour volume
source: year 2016, 2017, \& 2018 Automatic Traffic Recorders (ATR) Data ATR Stations:

2018: 7, 67, 171, 516, 520, 548, 773, 774
2017: 7, 67, 171, 516, 520, 773, 774, 548, 549
Ohio Department of Transportatio
Modeling \& Forecasting Section
June 2019
2016: 7, 67, 516, 520, 773, 774, 548, 549

## 2-Lane Highway Left Turn Lane Warrant

( $>40 \mathrm{mph}$ or 70 kph Posted Speed)



THE DISTILLERY TRAFFIC ACCESS STUDY

## 2-Lane Highway Right Turn Lane Warrant

> 40 mph or 70 kph Posted Speed


WARRANT SUMMARY

| ID | INTERSECTION [MOVEMENT] - VOLUME SET | AM PEAK <br> (A) | PM PEAK <br> (P) | RESULT |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
|  |  |  |  |  |
| 3 | Prop. Site Access \& SR 752 [EB RT] - 2023 'BUILD' | $(324,13)$ | $(404,42)$ | MET |
| 4 | Prop. Site Access \& SR 752 [EB RT] - 2033 'BUILD' | $(409,13)$ | $(502,42)$ | MET |
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2-Lane Highway Left Turn Lane Warrant ( $=<40 \mathrm{mph}$ or 70 kph Posted Speed)

WARRANT SUMMARY

| ID | INTERSECTION [MOVEMENT] - VOLUME SET | AM PEAK <br> (A) | PM PEAK <br> (P) |  | RESULT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Prop. Site Access \& SR 752 [WB LT]- 2023 'BUILD' | $(324,220 / 4.5 \%)$ | $(404,327 / 10.4 \%)$ |  | NOT MET |
| 2 | Prop. Site Access \& SR 752 [WB LT]-2033 'BUILD' | $(409,277 / 3.6 \%)$ | $(502,406 / 8.4 \%)$ |  | MET |
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THE DISTILLERY TRAFFIC ACCESS STUDY

## 2-Lane Highway Right Turn Lane Warrant $=<40 \mathrm{mph}$ or 70 kph Posted Speed


WARRANT SUMMARY

| ID | INTERSECTION [MOVEMENT] - vOLUME SET | AM PEAK <br> (A) | PM PEAK <br> (P) |  | RESULT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Prop. Site Access \& SR 752 [EB RT]- 2023 'BUILD' | $(324,13)$ | $(404,42)$ |  | NOT MET |
| 2 | Prop. Site Access \& SR 752 [EB RT]- 2033 'BUILD' | $(409,13)$ | $(502,42)$ |  | NOT MET |
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THE DISTILLERY TRAFFIC ACCESS STUDY
2-Lane Highway Left Turn Lane Warrant ( $=<40 \mathrm{mph}$ or 70 kph Posted Speed)

WARRANT SUMMARY

| ID | INTERSECTION [MOVEMENT] - VOLUME SET | AM PEAK <br> (A) | PM PEAK <br> (P) | RESULT |
| :---: | :---: | :---: | :---: | :---: |
| 2 | Prop. Site Access \& SR 752 [WB LT] - 2033165 UNIT 'BUILD' |  | (492,398 / 6.5\%) | NOT MET |
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THE DISTILLERY TRAFFIC ACCESS STUDY

## 2-Lane Highway Right Turn Lane Warrant

 > 40 mph or 70 kph Posted Speed

WARRANT SUMMARY


THE DISTILLERY TRAFFIC ACCESS STUDY

## 2-Lane Highway Left Turn Lane Warrant

( $>40 \mathrm{mph}$ or 70 kph Posted Speed)


| ID | INTERSECTION [MOVEMENT] - VOLUME SET | AM PEAK <br> (A) | PM PEAK <br> (P) | RESULT |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
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|  |  |  |  |  |
| 4 | Prop. Site Access \& SR 752 [WB LT] - 203370 UNIT 'BUILD' |  | (478,386 / 3.6\%) | NOT MET |
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THE DISTILLERY TRAFFIC ACCESS STUDY

## (1) PROP. SITE ACCESS \& SR 752 - WB LT - 2023 'BUILD' Critical Analysis Period: PM PEAK

Type $=$ Unsignalized Through Road
Speed = 50 MPH
Cycle Length = Turning Volume =

60 seconds
34 VPH
1
\# of Turning Lanes =
Advancing Volume $=$
327 VPH
Turning \% (>10\% HIGH) 10.4\% HIGH
Design Condition $=\quad \mathrm{B}$ or C
Vehicles per Cycle $=0.6$
Storage Length $($ Calc $)=50$ feet

Design Condition $($ Rev $)=$
Storage Length $($ Adj $)=\quad$ NA
Deceleration/Div. Taper $=225$ feet
Turn Lane Length $=\quad 225$ feet


Calculations based on 401-7E in ODOT
L\&D Manual. All dimensions are in feet.

## (2) PROP. SITE ACCESS \& SR 752 - WB LT - 2033 'BUILD' <br> Critical Analysis Period: PM PEAK

Type $=$ Unsignalized Through Road
Speed $=\quad 50 \mathrm{MPH}$
Cycle Length =
Turning Volume =
60 seconds
34 VPH
\# of Turning Lanes =
1
Advancing Volume $=406 \mathrm{VPH}$
Turning \% (>10\% HIGH) 8.4\% LOW
Design Condition $=\quad \mathrm{B}$
Vehicles per Cycle $=0.6$
Storage Length $($ Calc $)=50$ feet
(3) PROP. SITE ACCESS \& SR 752 - WB LT - 2023 'BUILD' Critical Analysis Period: PM PEAK

Type $=$ Unsignalized Through Road
Speed $=\quad 55 \mathrm{MPH}$
Cycle Length $=\quad 60$ seconds
Turning Volume $=\quad 34 \mathrm{VPH}$
\# of Turning Lanes = 1
Advancing Volume $=327 \mathrm{VPH}$
Turning \% (>10\% HIGH) 10.4\% HIGH
Design Condition $=\quad \mathrm{B}$ or C
Vehicles per Cycle $=0.6$
Storage Length (Calc) $=50$ feet


|  |  | 225 |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Storage Length $($ Adj $)=$ | NA |  |  |  |
| Deceleration/Div. Taper $=$ | 225 feet |  |  |  |
| Turn Lane Length $=$ | 225 feet | 50 |  |  |

Calculations based on 401-7E in ODOT
L\&D Manual. All dimensions are in feet.

## (4) PROP. SITE ACCESS \& SR 752 - WB LT - 2033 'BUILD' Critical Analysis Period: PM PEAK

Type = Unsignalized Through Road
Speed $=\quad 55 \mathrm{MPH}$
Cycle Length =
Turning Volume =
\# of Turning Lanes =
Advancing Volume $=$
Turning \% (>10\% HIGH) 8.4\% LOW
Design Condition $=\quad B$
Vehicles per $\mathrm{Cycle}=\quad 0.6$
Storage Length $($ Calc $)=50$ feet

Design Condition $($ Rev $)=\quad B$
Storage Length $(\operatorname{Adj})=$ NA
Deceleration/Div. Taper $=285$ feet
Turn Lane Length $=\quad 285$ feet


Calculations based on 401-7E in ODOT
L\&D Manual. All dimensions are in feet.


Calculations based on 401-7E in ODOT L\&D Manual. All dimensions are in feet.

## (2) PROP. SITE ACCESS \& SR 752 - EB RT - 2033 'BUILD' Critical Analysis Period: PM Peak

| Type $=$ Unsignalized T | rough | Road |  |  | Calculations based on 401-7E in ODOT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Speed = | 50 | MPH | Storage Length ( Adj ) $=$ | NA | L\&D Manual. All dimensions are in feet. |
| Cycle Length = | 60 | seconds | Deceleration/Div. Taper = | 225 feet |  |
| Turning Volume = | 42 | VPH | Turn Lane Length = | 225 feet |  |
| \# of Turning Lanes = | 1 |  |  |  | 7 7 |
| Advancing Volume $=$ | 502 | VPH |  |  |  |
| Turning \% (>10\% HIGH) | 8.4\% | LOW |  |  | 50 |
| Design Condition = | B |  |  |  |  |
| Vehicles per Cycle = | 0.70 |  |  |  | 225 |
| Storage Length (Calc) = | 50 | feet |  |  |  |

(4) PROP. SITE ACCESS \& SR 752 - EB RT - 2033 'BUILD'

## Critical Analysis Period: PM Peak

| Type $=$ Unsignalized Th | rough | Road |  |  | Calculations based on 401-7E in ODOT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Speed = | 55 | MPH | Storage Length ( Adj ) $=$ | NA | L\&D Manual. All dimensions are in feet. |
| Cycle Length = | 60 | seconds | Deceleration/Div. Taper = | 285 feet |  |
| Turning Volume = | 42 | VPH | Turn Lane Length = | 285 feet |  |
| \# of Turning Lanes = | 1 |  |  |  | 7 7 |
| Advancing Volume $=$ | 502 | VPH |  |  |  |
| Turning \% (>10\% HIGH) | 8.4\% | LOW |  |  | 50 |
| Design Condition = | B |  |  |  |  |
| Vehicles per Cycle = | 0.70 |  |  |  | 285 |
| Storage Length (Calc) = | 50 | feet |  |  |  |


[^0]:    *T: Thru

